

# SPE-GESGB CCUS Conference 2023

## 3-6 October 2023, Virtual

CO<sub>2</sub> Injectivity Review

*by*

Irfan Sami

Gaffney  
Cline



# Disclaimer Statement

The material and views expressed in this presentation are those of the author.

The presentation material has been prepared responsibly and carefully, but no warranty, expressed or implied, is given that the information is complete or accurate nor that it is fit for a particular purpose. All such warranties are expressly disclaimed and excluded.

Attendees are urged to obtain independent advice on any matter relating to the interpretation of CO<sub>2</sub> injection operations and injectivity estimation.

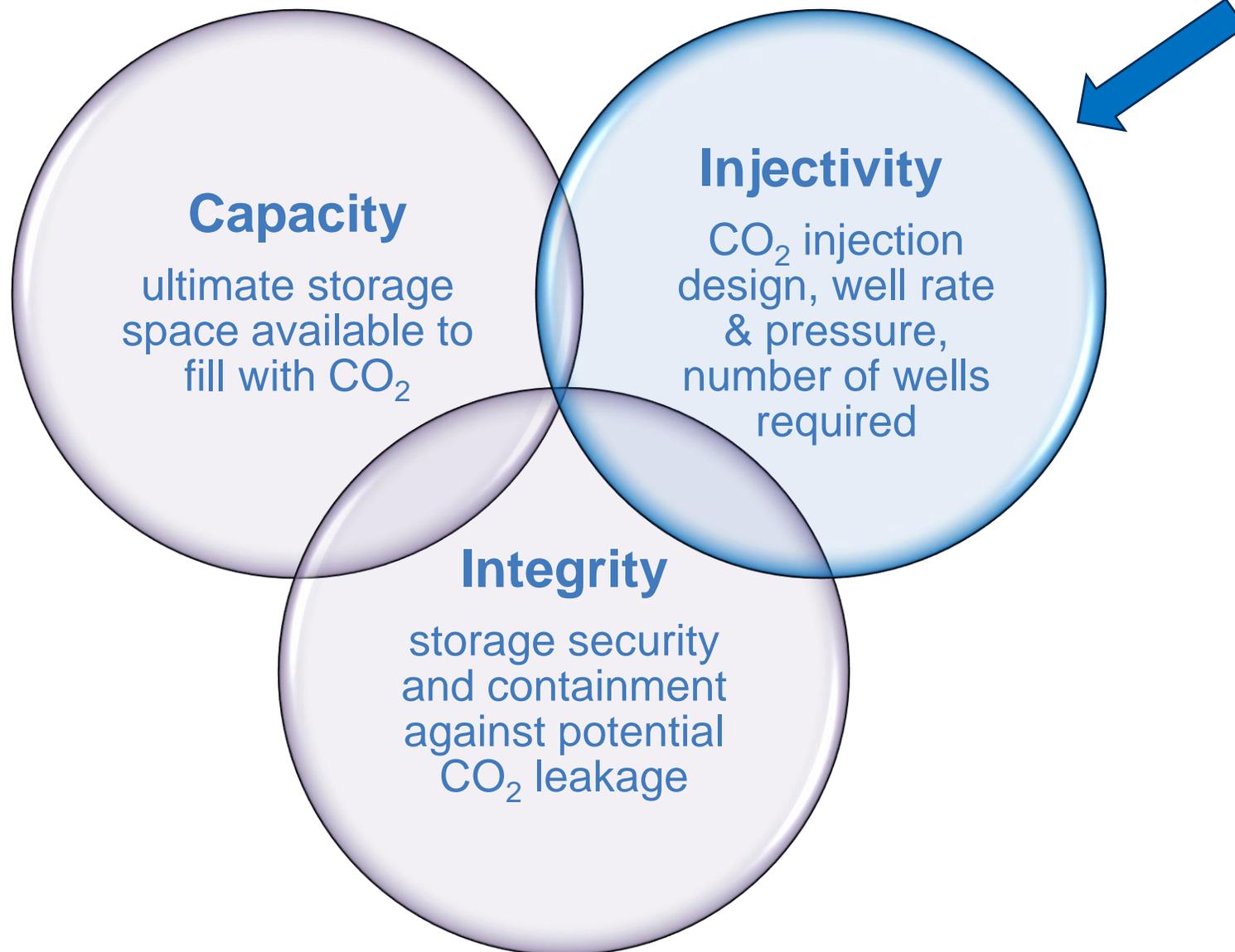
© 2023 GaffneyCline. All rights reserved. Terms and conditions of use: by accepting this document, the recipient agrees that the document together with all information included therein is the confidential and proprietary property of GaffneyCline and includes valuable trade secrets and/or proprietary information of GaffneyCline (collectively "information"). GaffneyCline retains all rights under copyright laws and trade secret laws of the United States of America and other countries. The recipient further agrees that the document may not be distributed, transmitted, copied or reproduced in whole or in part by any means, electronic, mechanical, or otherwise, without the express prior written consent of GaffneyCline, and may not be used directly or indirectly in any way detrimental to GaffneyCline's interest.

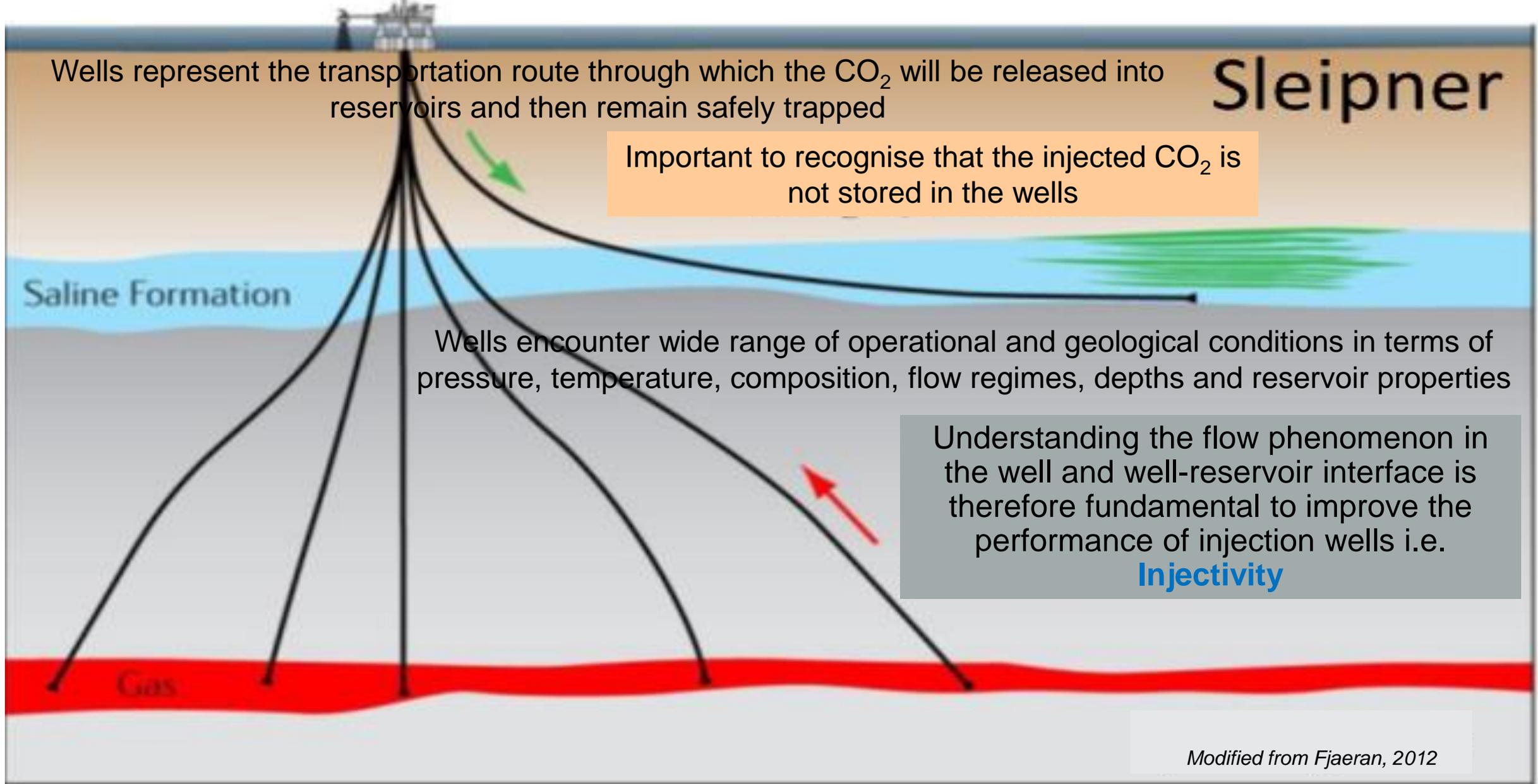
# Speaker Bio

- Reservoir Engineer.
- 23+ year industry experience with leading international energy companies and consultancies working on projects related to reservoir engineering, field development planning, data-room due diligence and CO<sub>2</sub> storage.
- Currently with GaffneyCline as Principal Advisor – Reservoir Engineering.
- CCS projects experience:
  - Studies involving:
    - Simulation modelling studies;
    - CO<sub>2</sub> storage evaluation studies;
    - Peer reviews.
  - Geographical spread:
    - North Sea;
    - Eastern Mediterranean;
    - Irish Sea;
    - Middle East;
    - Sarawak basin, offshore Malaysia.
- Irfan has an M.S. in Petroleum Engineering from KFUPM in Dhahran, Saudi Arabia and a B.Eng. from NED University in Karachi, Pakistan.



# CO<sub>2</sub> Storage – Key Links





Wells represent the transportation route through which the CO<sub>2</sub> will be released into reservoirs and then remain safely trapped

# Sleipner

Important to recognise that the injected CO<sub>2</sub> is not stored in the wells

Saline Formation

Wells encounter wide range of operational and geological conditions in terms of pressure, temperature, composition, flow regimes, depths and reservoir properties

Understanding the flow phenomenon in the well and well-reservoir interface is therefore fundamental to improve the performance of injection wells i.e. **Injectivity**

Gas

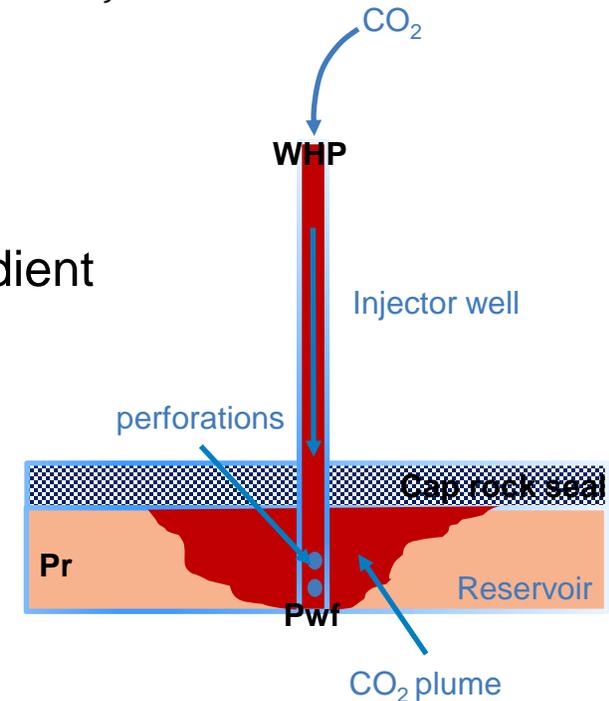
*Modified from Fjaeran, 2012*

# Injectivity – What is it & What Controls it?

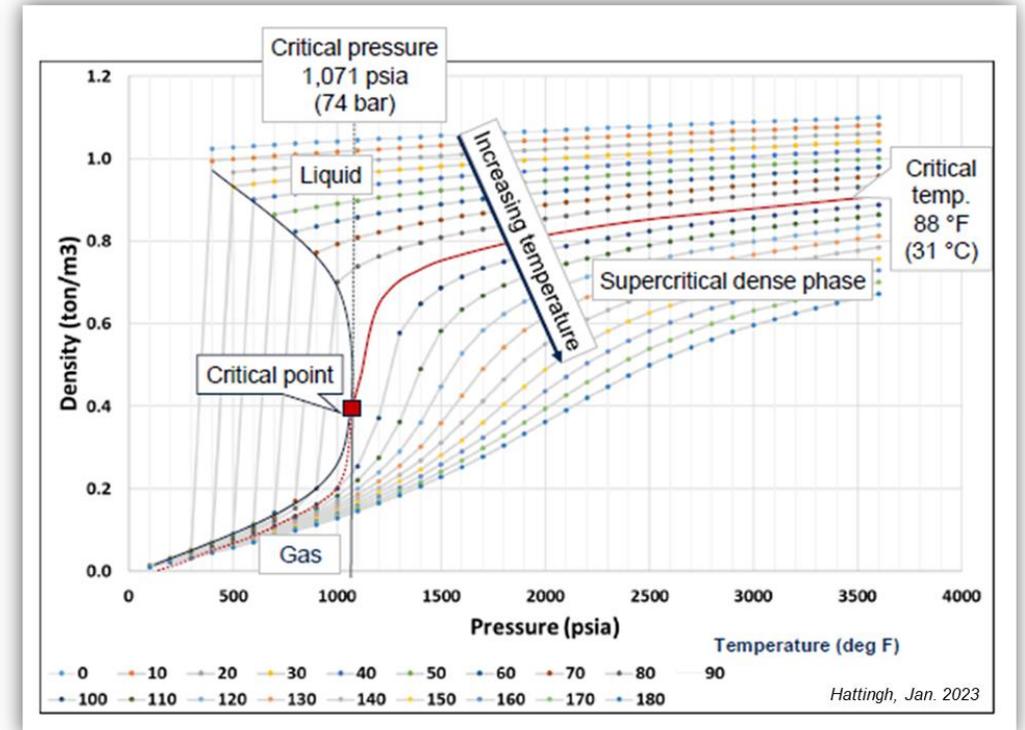
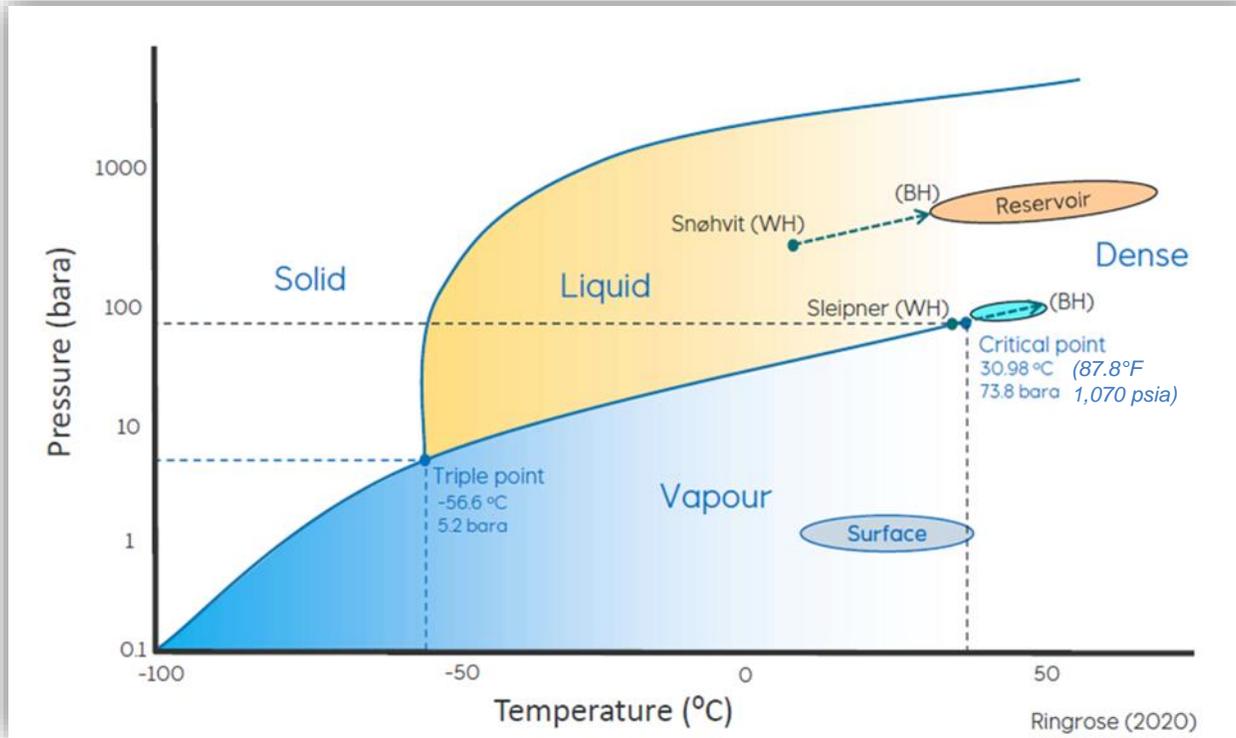
- Injectivity:
  - Ability to push the CO<sub>2</sub> through the matrix in the storage pore space
  - Relates injection rate to pressure difference between the injection well and the reservoir

$$q = \frac{2\pi khT}{p_1 T \ln(r_2/r_1)} \int_{p_1}^{p_2} \frac{\tilde{p} d\tilde{p}}{\mu_g(\tilde{p})z(\tilde{p})} \quad \text{or in simple terms} \quad \text{Injectivity} = \frac{q}{\Delta p} \quad \text{where } \Delta p = P_{wf}^2 - P_r^2$$

- Controlling factors:
  - Amount and the quality of the injected CO<sub>2</sub>
  - Reservoir conditions like pressure & temperature
  - Maximum allowable injection pressure governed by fracture pressure gradient
  - Reservoir characteristics like permeability and net pay thickness
  - Reservoir transmissibility, connectivity and relative permeability
  - Influences like heterogeneities/shale layers in the reservoir
  - Length of perforation interval and near wellbore damage (skin)
  - Near wellbore pore scale rock arrangement (matrix/natural fractures)
  - Salt precipitation/dry-out effects



# CO<sub>2</sub> Properties



- In supercritical phase - not possible to distinguish liquid from vapor with viscosity of a gas but density of a liquid.
- Near the critical point, small changes in operating conditions lead to large changes in physical properties particularly density.
- Reservoir pressure range ~83 – 140 bar (840 – 1,400 m depth) recommended to lead to an efficient utilization of storage volume.

# Injectivity - Depleted Fields Vs Saline Aquifers

## Depleted Fields

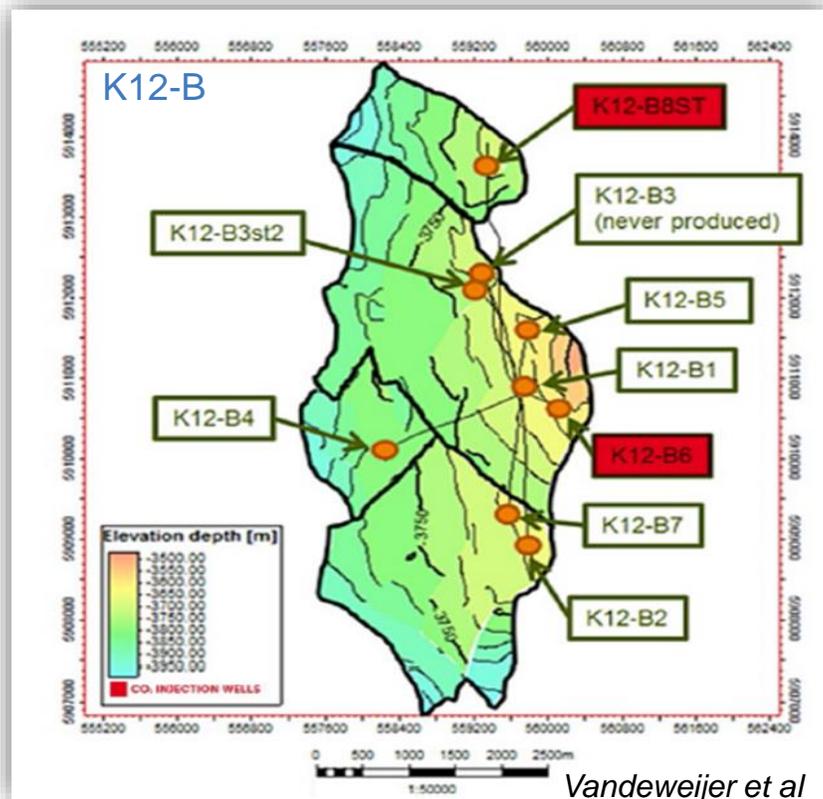
- Potentially high injectivity opportunity due to low initial pressures
- Phase change - in wellbore or near wellbore region
- Large density changes expected
- Bottomhole pressure response affected
- Possibly unstable well conditions
- Joule Thompson cooling
- Erosion risks due to increased velocity
- Risk of hydrate or ice formation

## Saline Aquifers

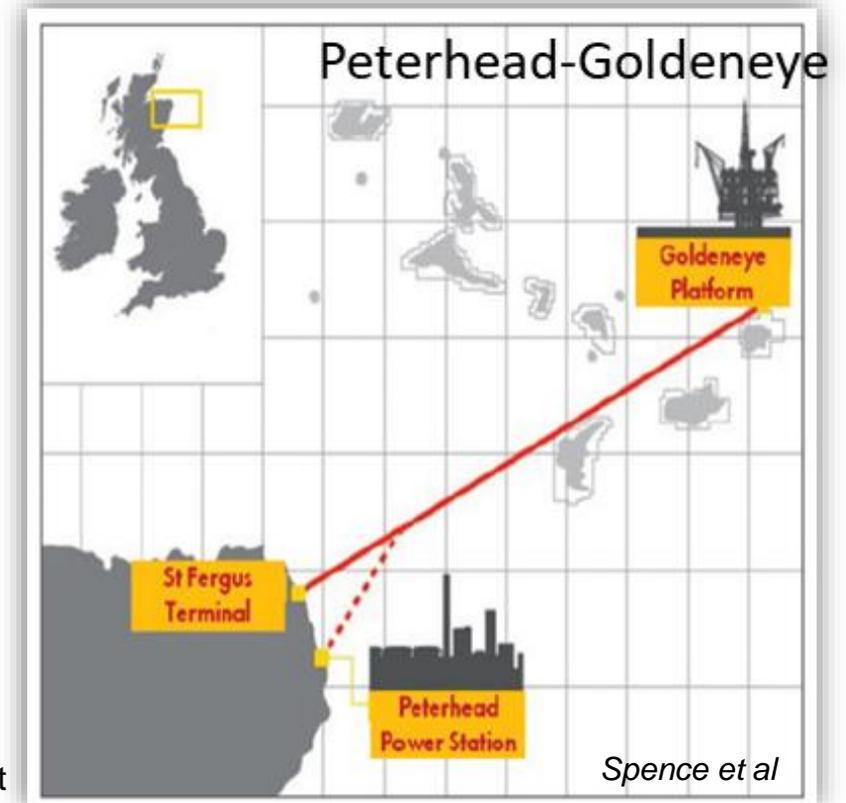
- CO<sub>2</sub> injection starts in high pressure environment
- Maintaining single phase (supercritical) condition is usually not an issue
- However, injecting against a high back pressure in the reservoir requires higher bottomhole pressure
- CO<sub>2</sub> has to work against a higher density fluid (water) that already occupies the pore space
- Risk of near wellbore dry-out effects
- Risk of breaching allowable pressure limit

# Depleted Fields – Global Experience

- CO<sub>2</sub> EOR targeting tertiary oil recovery from depleted oil fields has long been established
- However, projects exclusively aiming for CO<sub>2</sub> storage in depleted oil and gas fields are still few
- Pilot projects like Otway (Australia), Rouse (France) and K12-B (Netherlands) present some first-hand experiences
- Others in planning/feasibility stages provide useful public domain information (Peterhead/Goldeneye, ROAD, etc.)

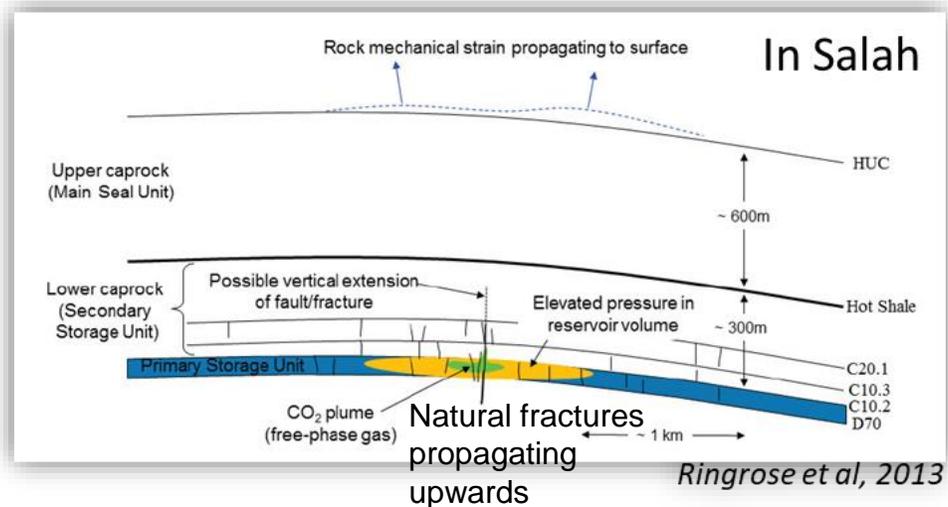


- **At K12-B**, CO<sub>2</sub> stripped from produced gas (13% CO<sub>2</sub>) and re-injected into depleted gas reservoir between 2004-2017 (total 0.1 Mt CO<sub>2</sub> injected)
- Injection operations involved phase changes in the wellbore and in the reservoir
- However, K12-B field CO<sub>2</sub> injection continued without any major complications
- Depleted gas field '**Goldeneye**' (offshore UK) was selected for the Peterhead CCS project aiming to inject 1 MTPA for 15 years
- Four Goldeneye legacy wells were planned to be re-fitted for CO<sub>2</sub> service
- Strong aquifer drive during production phase meant that water was expected at the sand face initially

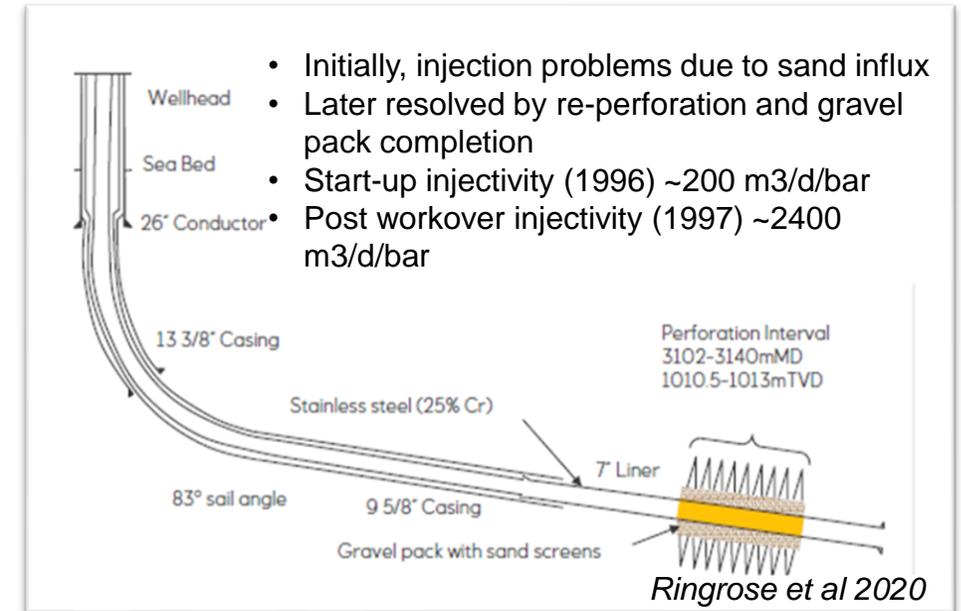


# Saline Aquifers – Global Experience

- Most large-scale operational CCS projects have used saline aquifers as storage formations
- Sleipner (offshore Norway) - operational since 1996, annual CO<sub>2</sub> injection rate 1 Mt
- In Salah (onshore Algeria) – CO<sub>2</sub> injection into the down-dip aquifer of the Krechba SS
- Snøhvit LNG project in the Barents Sea (Norway) – Saline aquifer



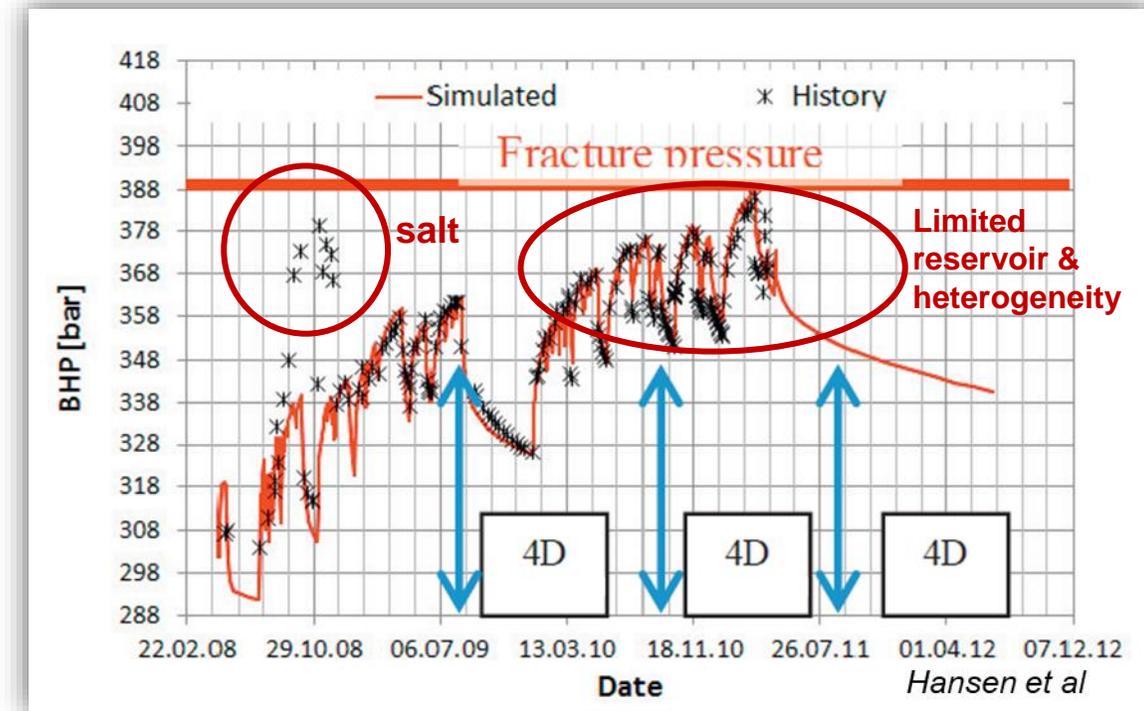
Sleipner CO<sub>2</sub> injection well 15/9-A16



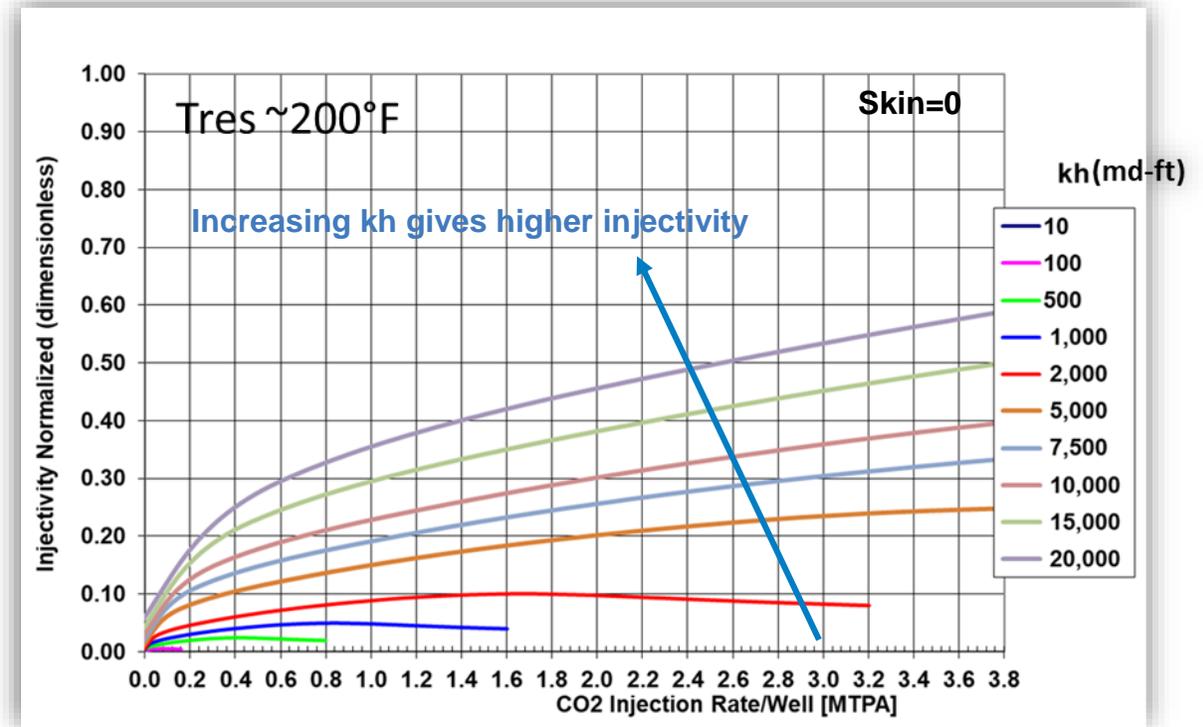
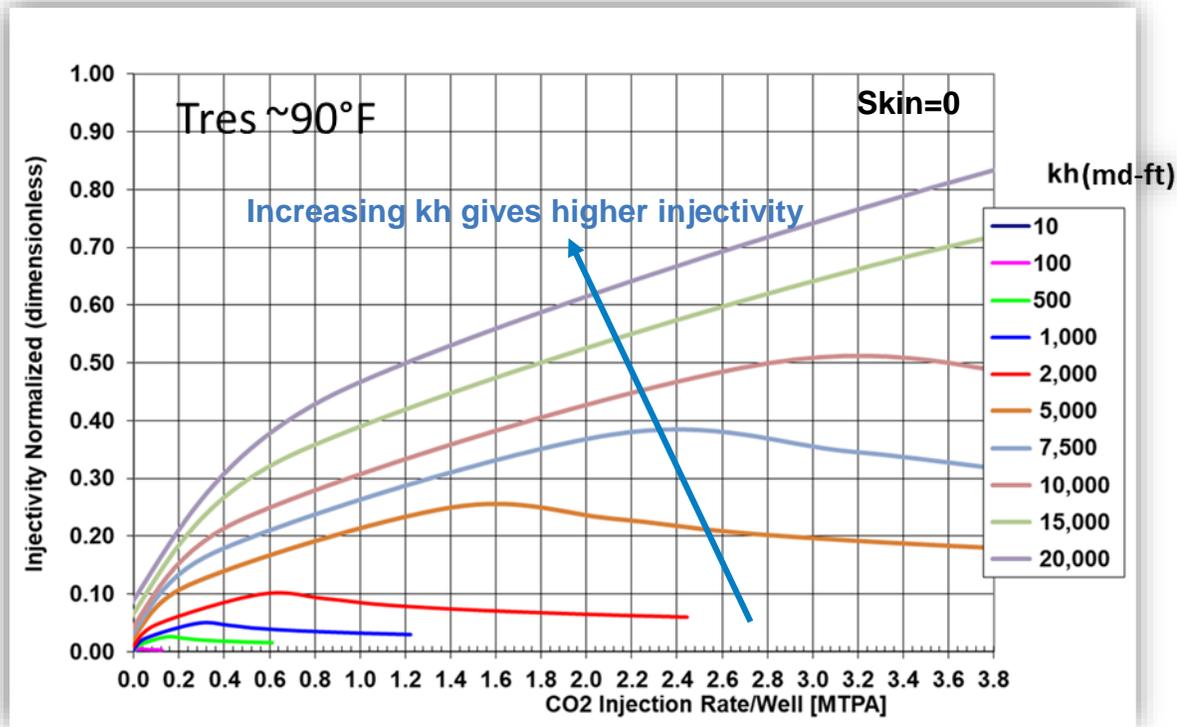
# Saline Aquifers – Snohvit Experience

- Snohvit project injected 1.6 Mt of CO<sub>2</sub> between 2008 – 2012 in the Tubåen formation
- 110 m thick formation, depth 2.7-2.8 km, initial conditions of Pres 285 bar, Tres 98°C
- Pressure build-up observed and injection stopped
- Initially salt precipitation in the near wellbore formation was suspected and treated by MEG injection
- Followed up with PLTs and reperforations; subsequent injection again led to continued pressure rise
- Studies/investigations showed that this pressure build-up was mainly caused by limited reservoir volume and formation heterogeneity
- Reservoir heterogeneities and connectivity across faults mean the effective permeability of the Tubåen formation units around the injector well was much lower
- Eventually, injection was diverted to another target formation, as the required injection rate could not be accommodated by the near well reservoir in the Tubåen

Reservoir Unit	Core porosity average (%)	Core permeability average (mD)	Approximate k.H in perforated interval [mD.m]
Tubåen 3	12.32	114	2400
Tubåen 2	7.44	362	550
Tubåen 1	19.75	7650	40000



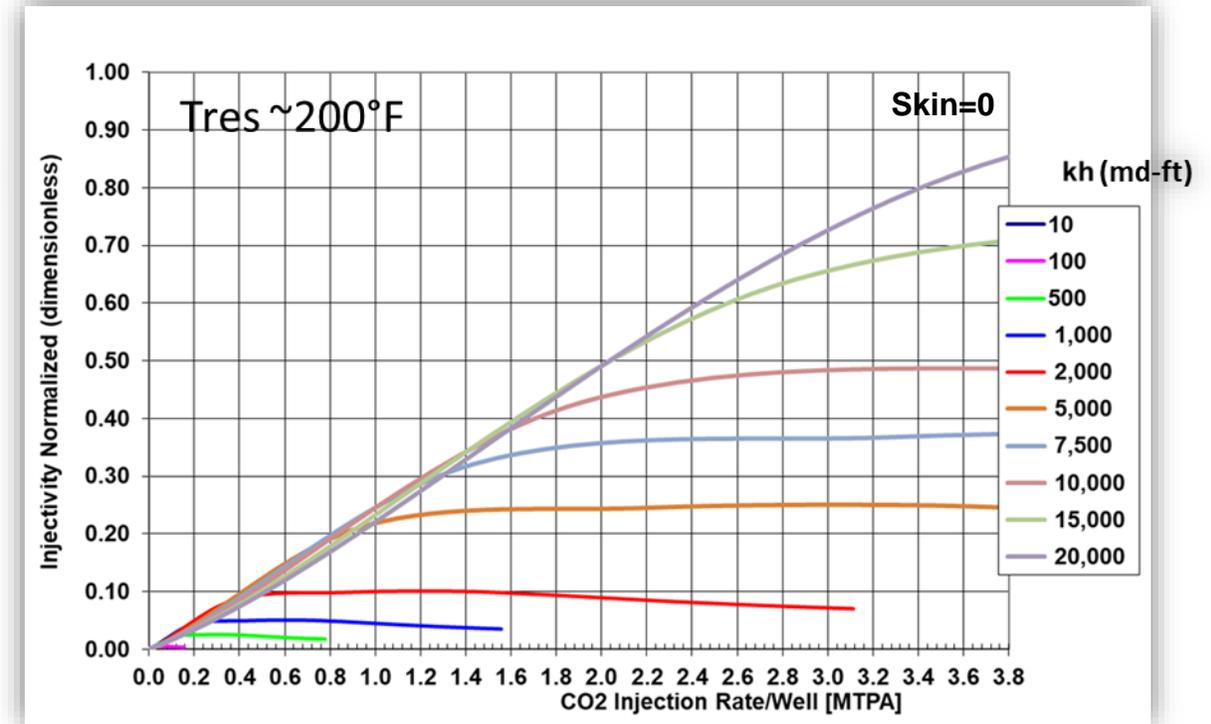
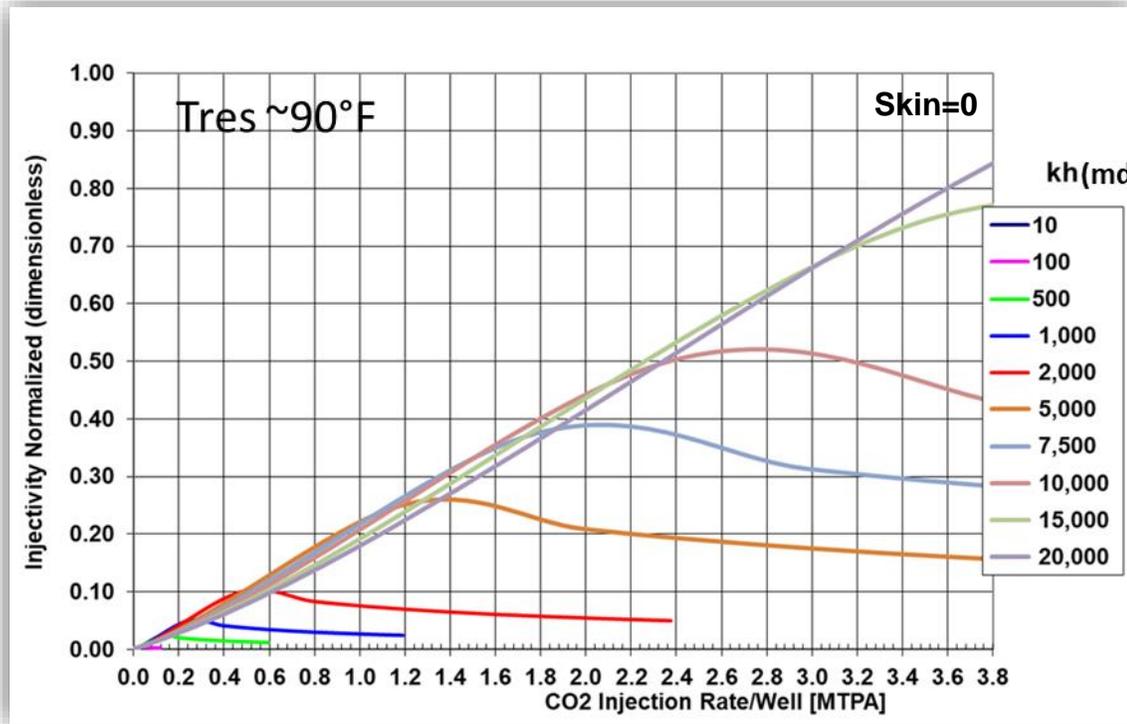
# Injectivity – Strongly Depleted Reservoir Conditions (Pres ~15bar)



*Injectivity estimate (Y-axis) has been standardized by normalizing with the maximum injectivity obtained*

- Better reservoir quality (higher kh) results in improved injectivity at all reservoir PT conditions
- Injectivity increases when bottomhole injection pressure is below critical pressure
- While it decreases and then stabilizes as BH pressure rises above critical pressure
- At higher temperature, injectivity shows a smooth increasing trend but is smaller than that at lower temperature
- Changing density and viscosity behaviour of CO<sub>2</sub> below and above critical point causes the above phenomenon

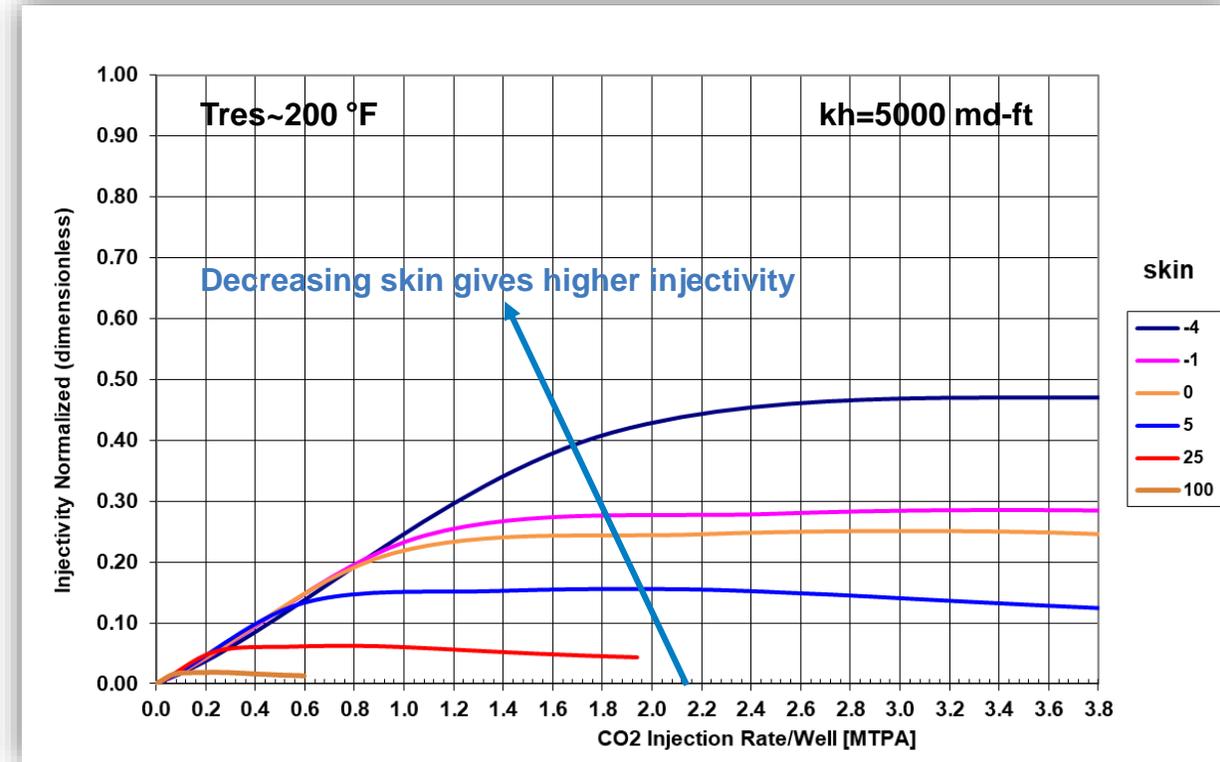
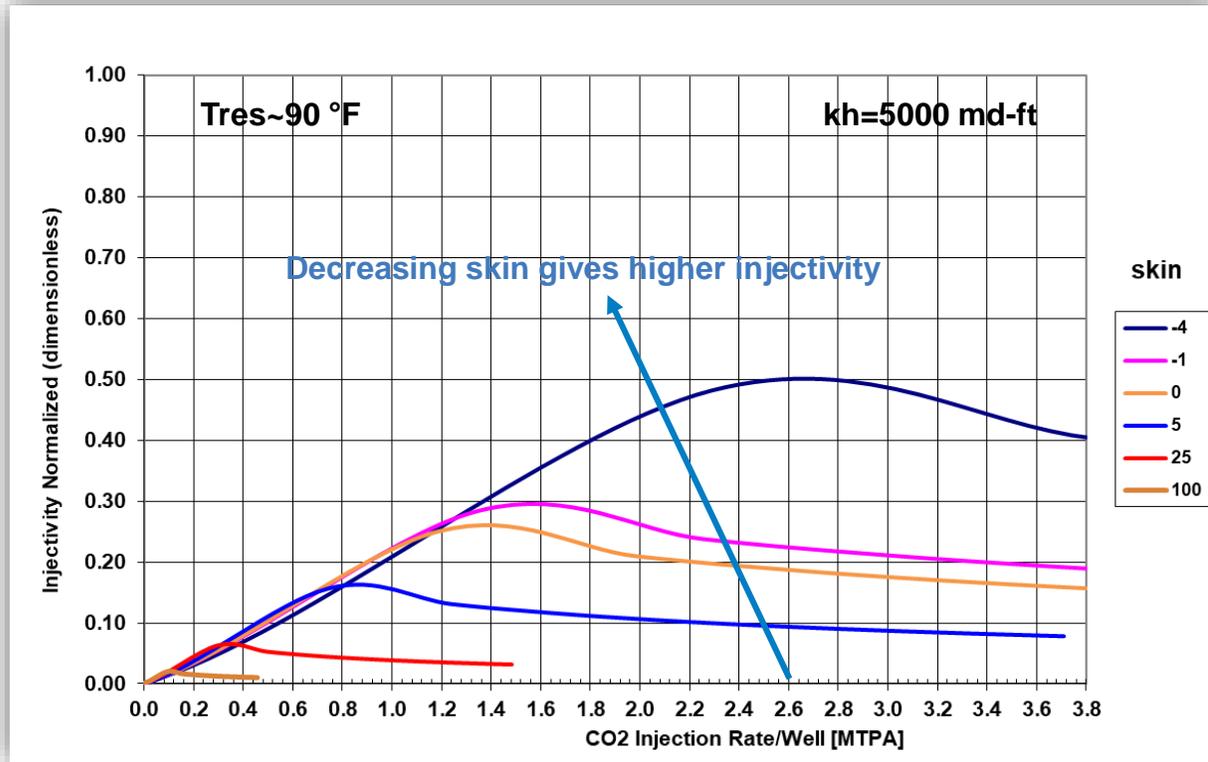
# Injectivity – Near Critical Reservoir Conditions (Pres ~70 bar)



*Injectivity estimate (Y-axis) has been standardized by normalizing with the maximum injectivity obtained*

- As reservoir pressure increases and nears the critical pressure, injectivity aligns to a linear positive trend
- At higher temperature, injectivity again shows a smooth rising trend that later stabilizes
- As reservoir pressure increases further (to typical un-depleted level), injectivity changes are small; main limiting factor being the maximum allowable injection pressure constraint at the bottomhole

# Injectivity – Skin Sensitivity (Pres ~70 bar)

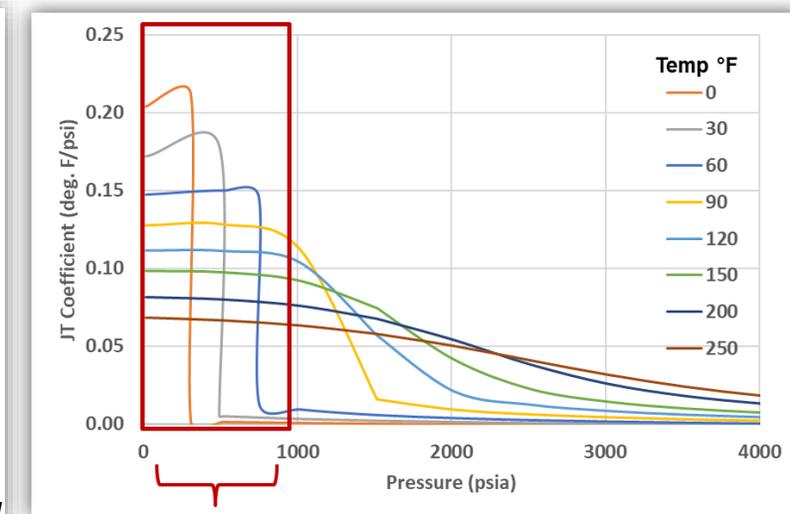
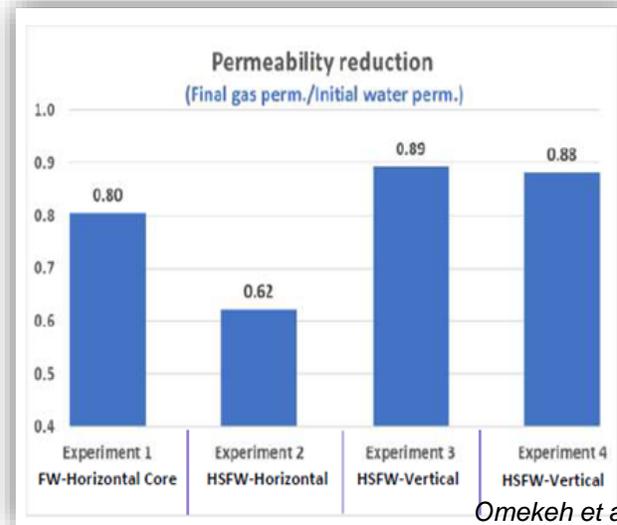
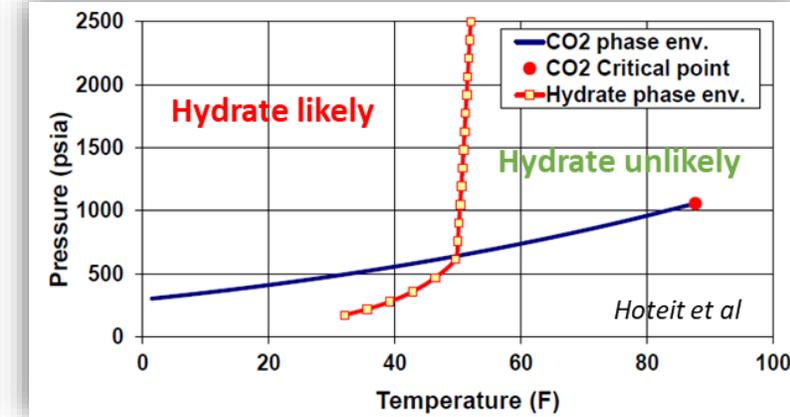


*Injectivity estimate (Y-axis) has been standardized by normalizing with the maximum injectivity obtained*

- Decreasing skin implies lower damage around wellbore and leads to lower pressure differential between the bottomhole and the reservoir for the same injection rate resulting in higher injectivity

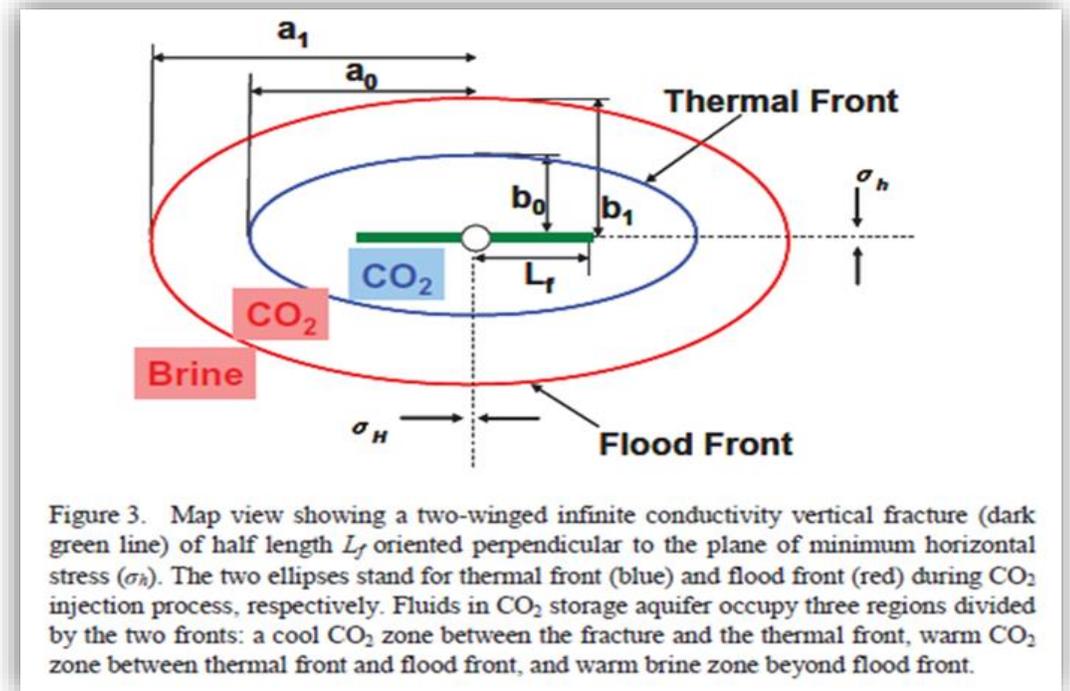
# Flow Assurance Issues Impacting Injectivity

- Joule Thomson Cooling – cooling effect as the fluid expands up the well or into the reservoir
- Hydrates - Loss of flow due to hydrate formation at the wellhead or across perforations
- Dry supercritical carbon dioxide can evaporate saline water in rock pores and precipitate salt leading to impairment of injection rates
- Pore space blockage due to hydrate/ice formation, salt precipitation – acts like a positive skin effect and reduces injectivity



# Thermally Induced Fractures During CO<sub>2</sub> Injection

- Thermal fracturing in the near wellbore area due to sharp temperature reduction
- Temperature effects reduce the fracture critical pressure and induce near wellbore fractures
- Slow growth fracture can increase injectivity without changing flood region shape
- Fast propagation fractures increase injectivity but stretch flood region very flat
- Optimum fracture growth enhances permeability around the wellbore and increases injectivity



*Lou and Bryant*

# Summary

## Injectivity

- Ability to push the CO<sub>2</sub> through the rock matrix
- Controlled by various reservoir, fluid and operating parameters
- Determines number of injection wells required; big impact on any CCS project economics and feasibility

## Depleted Fields

- High injectivity potential due to large available pressure differential
- Suffer from phase change related challenges which can reduce injectivity

## Saline Aquifers

- Dense phase injection and therefore abrupt phase change issues are avoided
- High back pressures in the reservoir from the beginning leading to decreased injectivity

## Impact Factors

- Permeability-thickness (kh) and formation damage (skin)
- Others include heterogeneity, limited drainage area and connectivity

## Ways to Improve

- Optimized utilization of high perm reservoir zones and perforation intervals
- Matrix stimulation, rock fracture growth optimization, etc.
- Pressure management

# References

- Fjaeran, 'Mapping of Geological CO<sub>2</sub> Storage sites – an overview', CCOP EPPM Seminar, Bali, Indonesia, 2012
- Ringrose et al, 'CO<sub>2</sub> injection operations: Insights from Sleipner and Snøhvit', SPE CCUS Conference, Oct-2020
- Vandeweyer et al, '13 Years Of Safe CO<sub>2</sub> Injection At K12-B', EAGE Conference Nov-2018
- Underschultz et al, 'CO<sub>2</sub> storage in a depleted gas field: An overview of the CO<sub>2</sub>CRC Otway Project and initial results', International Journal of Greenhouse Gas Control 5, 2011
- Hansen et al, 'Snøhvit: The history of injecting and storing 1 Mt CO<sub>2</sub> in the fluvial Tubåen Fm.', Energy Procedia 37, 2013
- Ringrose et al, 'The In Salah CO<sub>2</sub> storage project: lessons learned and knowledge transfer', Energy Procedia 37, 2013
- Hattingh, 'Carbon Capture and Storage - Quantifying Geological Storage', SPE London Section Presentation, 2023
- Hoteit et al, 'Assessment of CO<sub>2</sub> Injectivity During Sequestration in Depleted Gas Reservoirs', Geosciences, 2019
- Spence et al, 'The Peterhead-Goldeneye gas post-combustion CCS project', Energy Procedia 63, 2014
- Xu et al, 'A CO<sub>2</sub>-Rich Gas Well Test and Analyses', Proceedings of the Asia Pacific Oil and Gas Conference and Exhibition, Jakarta, Indonesia, Oct-Nov 2007
- Ajayi et al, 'A review of CO<sub>2</sub> storage in geological formations emphasizing modelling, monitoring and capacity estimation approaches', Petroleum Science 16, 2019
- Lou and Bryant, 'Impacts of Injection Induced Fractures Propagation in CO<sub>2</sub> Geological Sequestration – Is Fracturing Good or Bad for CO<sub>2</sub> Sequestration', Energy Procedia 63, 2014

# Thank You

Acknowledgements

Event Audience

References

SPE/PESGB & GaffneyCline/BH

# Gaffney Cline